

Compatibility Characterization of Reclaimed Asphalt Pavement, Binder, and Recycling Agents in Asphalt Mixtures

Shubham H. Modi, Eshan V. Dave, Jo E. Sias, Zheng Wang

University of New Hampshire

Hassan Tabatabaee, Tony Sylvester

Cargill Bioindustrial

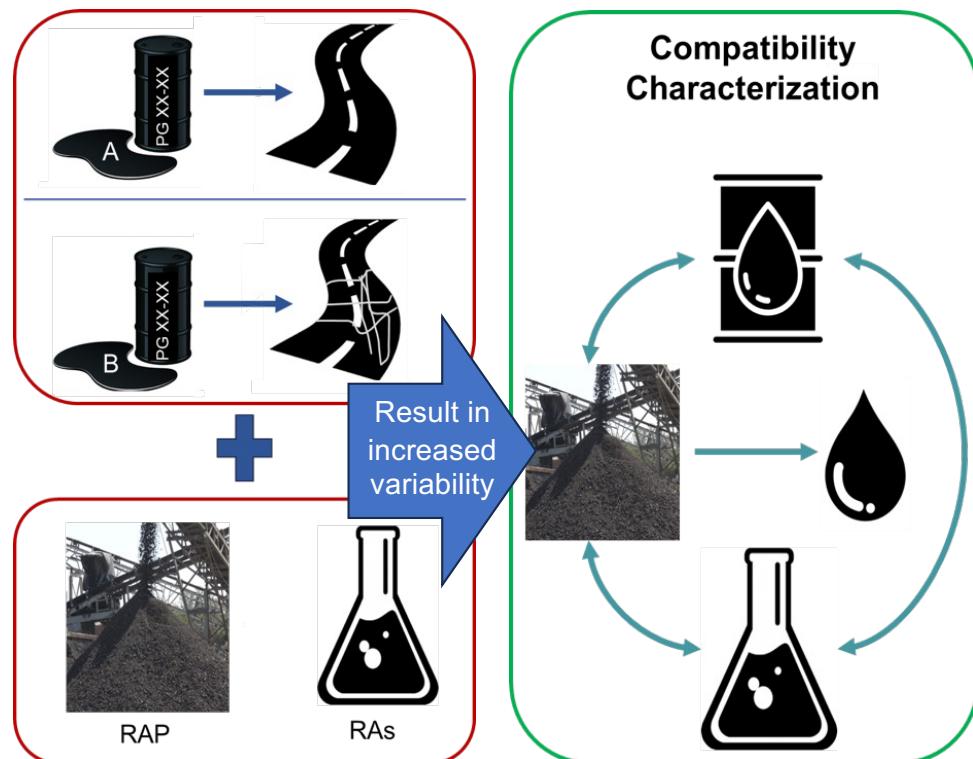
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Goal and Study Objectives

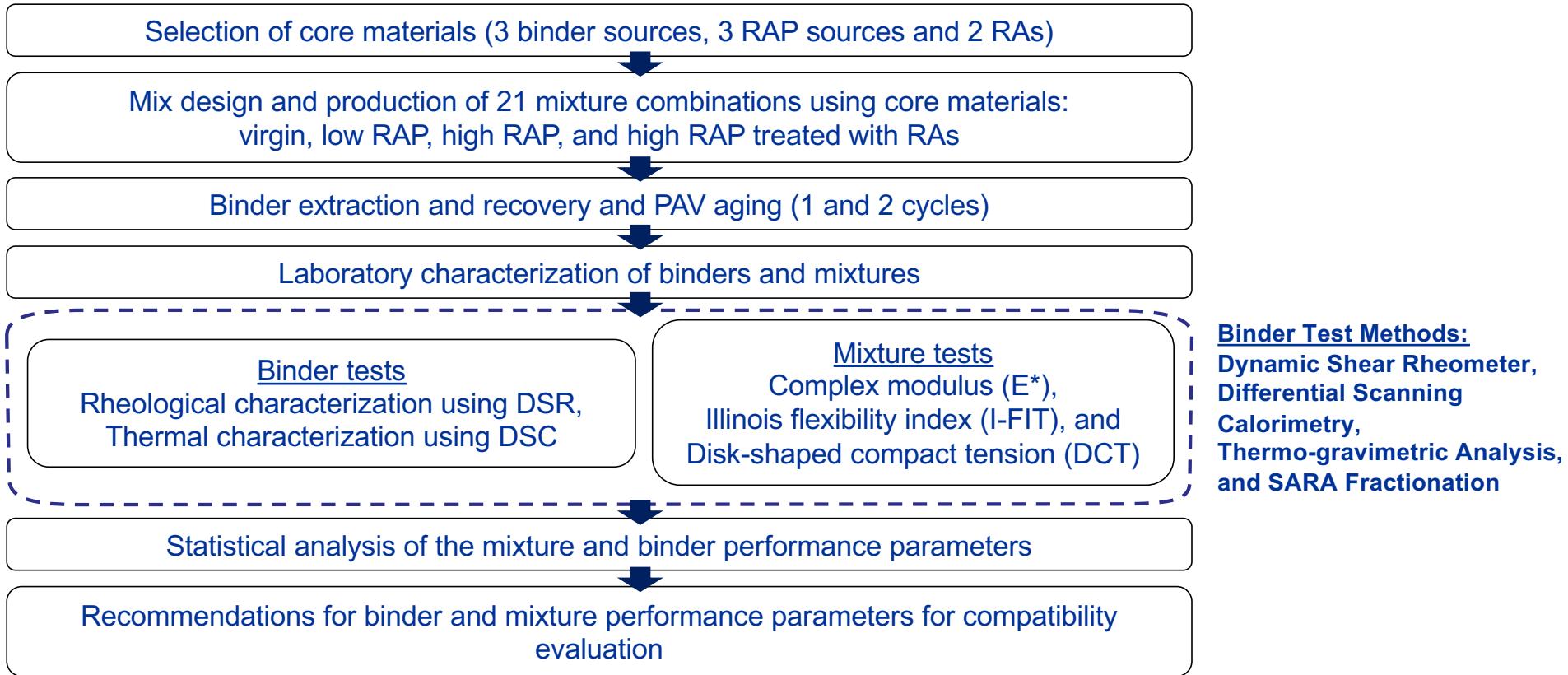
Motivation



Objective:

- Develop a practical and implementable compatibility characterization system:
 - Combination of various asphalt sources (*virgin binders, recycled asphalt binders*)
 - Combination of asphalt binders (*virgin, recycled*) with recycling agents

Research Approach



Binder Evaluation and Material Matrix

- **Binder Material**

- 27 binder blends
 - 3 virgin binders
 - 3 LRAP and 7 HRAP blends
 - 14 RA-treated HRAP blends

- **Three Aging Level**

- As-extracted
- 1 × PAV
- 2 × PAV

- **Test Methods**

- Dynamic shear rheometer
- Differential scanning calorimetry



Material Type	Material ID	Binder Grade (PG)	Source
RAP (graded as extracted)	1	103.1-4.6	Minnesota, US
	2	103.8-5.8	Alabama, US
	3	87.2-26	Texas, US
Binders	A	58-28	Minnesota, US
	B	64-22	Alabama, US
	C	64-22	Wisconsin, US
Recycling Agents	RA1	--	Bio-based
	RA2	--	Petroleum-based



Mixture Evaluation Methods

- **Mix Design**

- 21 mixtures (3 virgin mixtures, 3 LRAP mixtures, 9 HRAP mixtures, 6 RA treated mixtures)
- **Similar gradation and comparable volumetrics**

- **Mixture Tests**

- Complex Modulus (AASHTO T 342)
- Disk-Shaped Compact Tension (DCT) Test (ASTM D7313)
- Illinois Flexibility Index Test (AASHTO T 393)



Complex Modulus



DCT

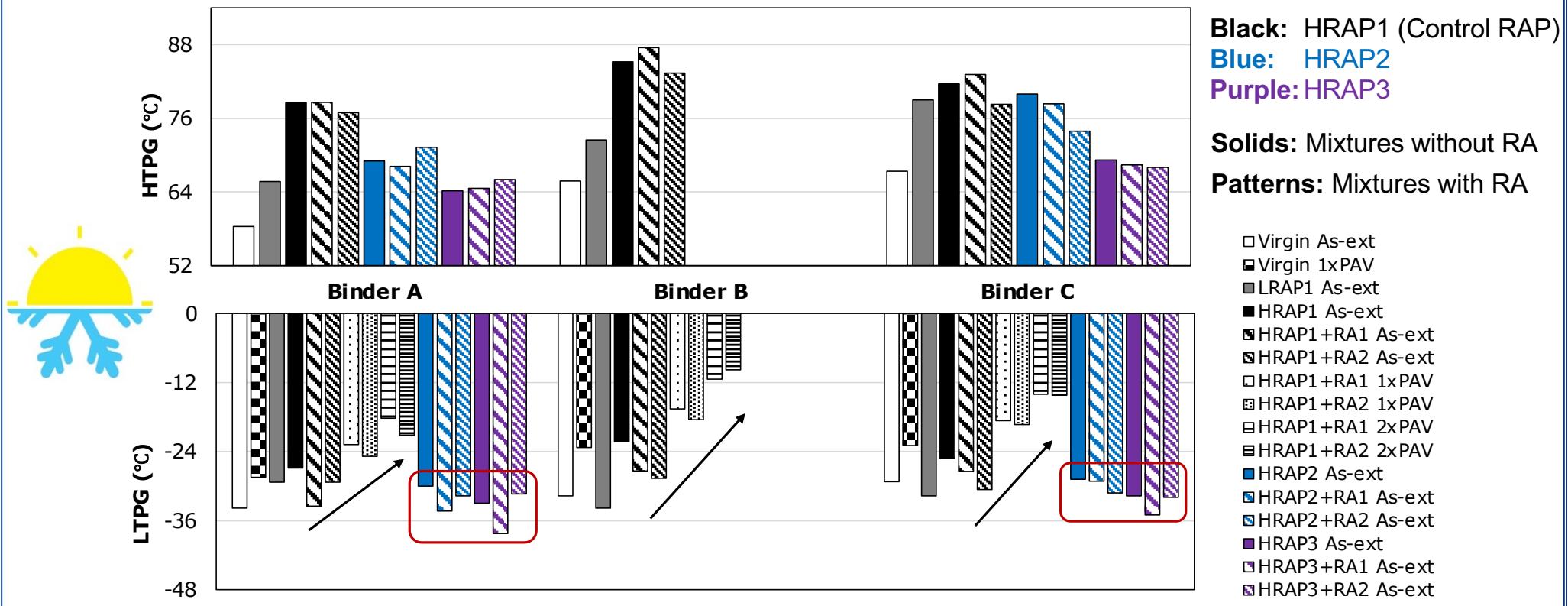
I-FIT



*Part 1 : Binder Testing Results
(Rheological and Thermal Analysis)*



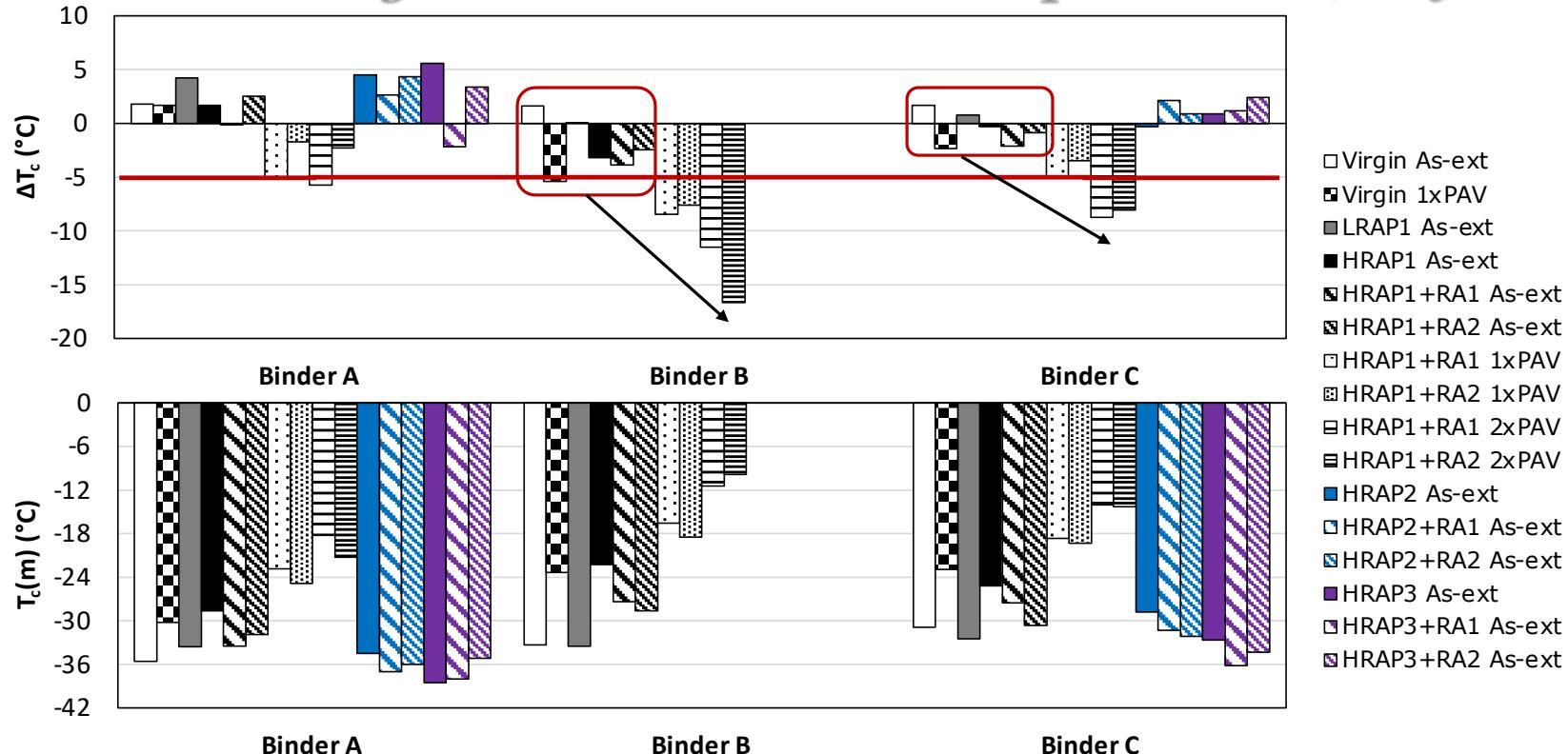
Continuous PG



- Inclusion of RA results in small variation in HTPG
- RAP1 blends have the warmest LTPG with all binders among all RAP materials
- Binder B has higher aging susceptibility than Binder C



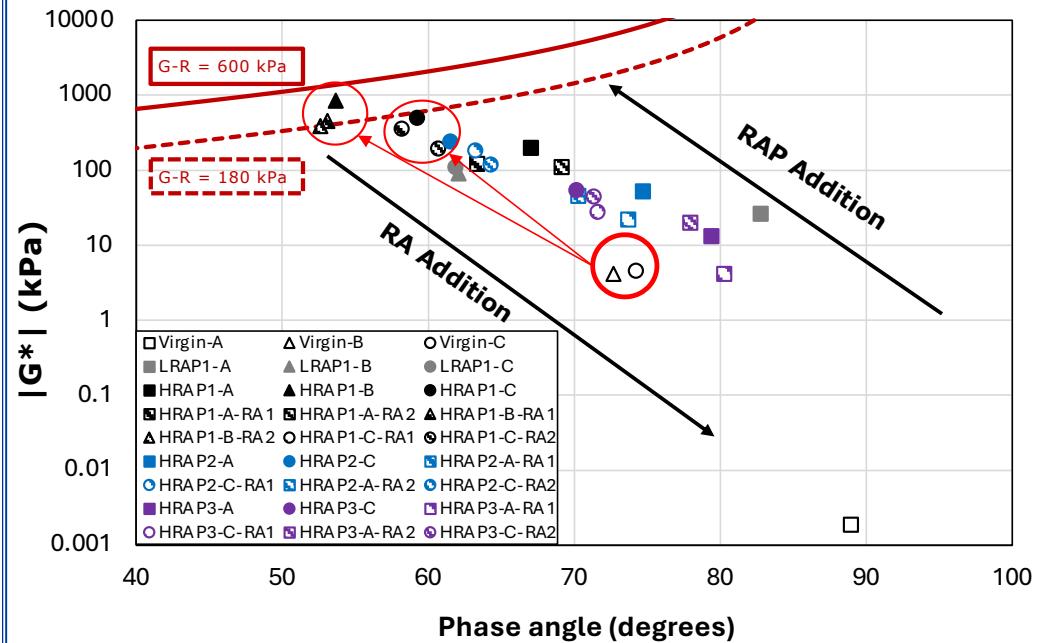
Change in Critical Low Temperature (ΔT_c)



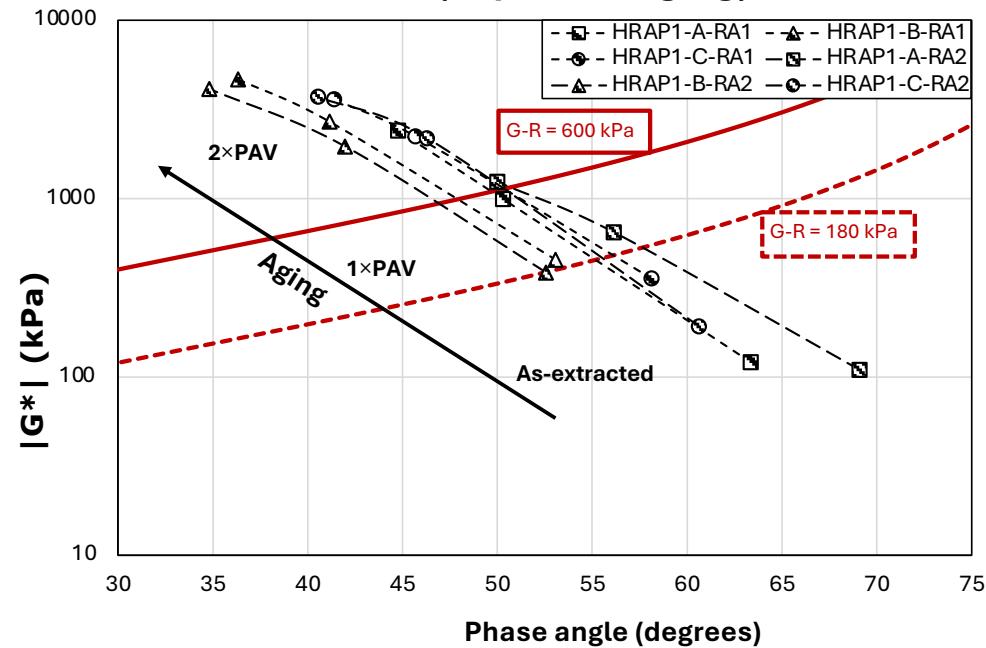
- Binder B blends show poor ΔT_c values and the severe impact of aging (both B and C have similar PG)
- ΔT_c is a composite parameter and trends with ΔT_c should be evaluated in conjunction with $T_c(m)$

Black Space Analysis (@15 °C and 0.005 rad/sec)

All extracted (Impact of Rejuvenation)



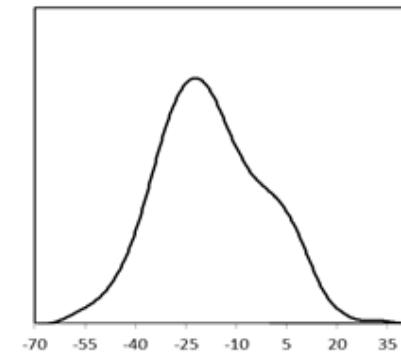
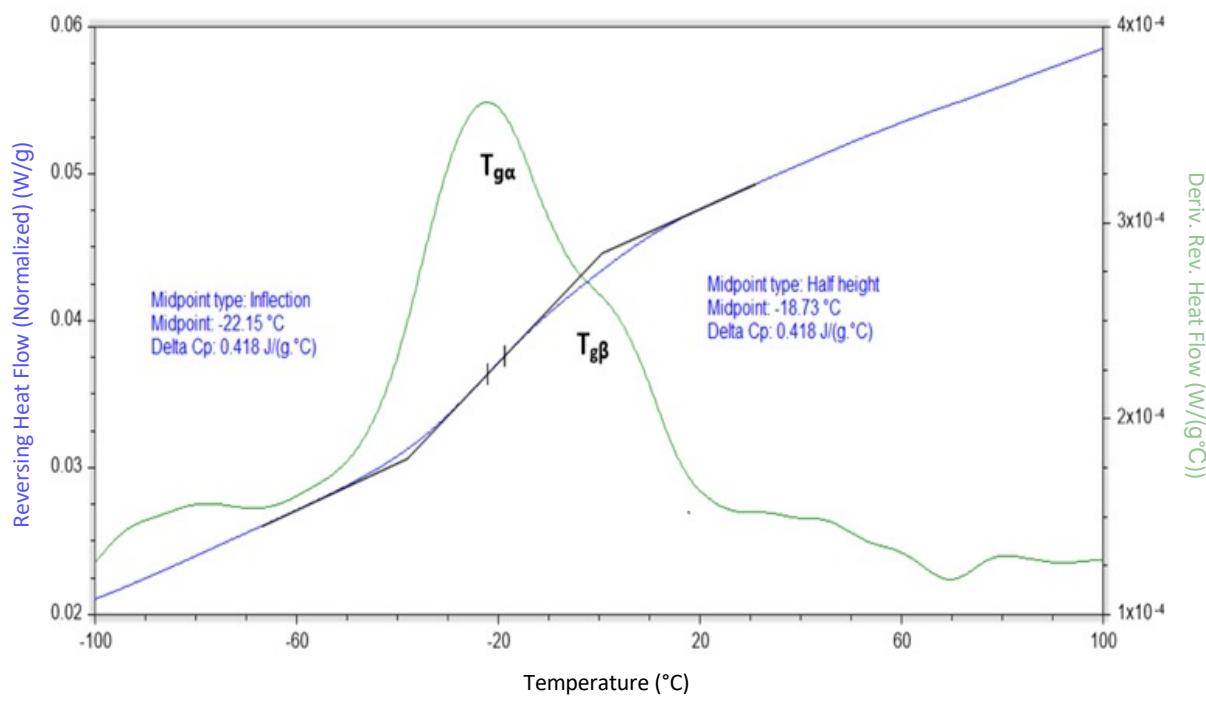
RAP-1 (Impact of Aging)



- Binder B blends exceed the warning limit and indicate potential incompatibility with both RAs
- Binder B blends have poor properties after all aging levels

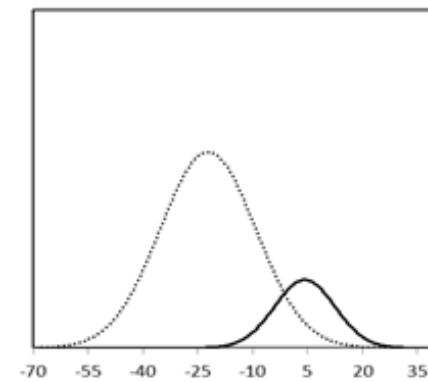


DSC Thermal Analysis: Parameters



Deconvolution

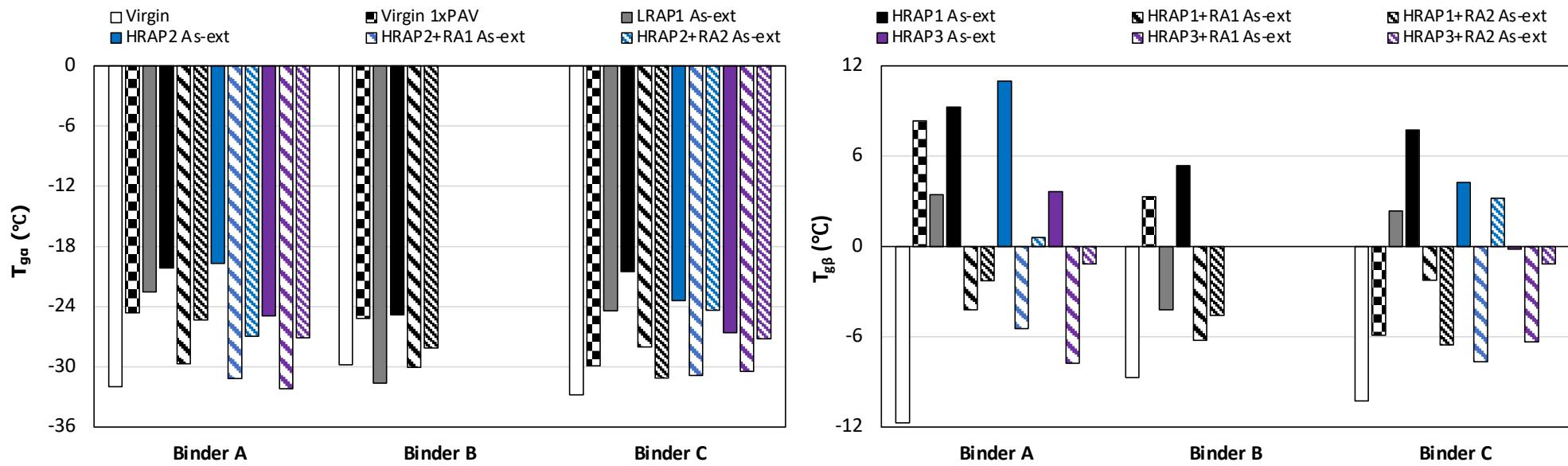
— $T_{g\beta}$ $T_{g\alpha}$



$$\phi_{\alpha,\beta} = \frac{\Delta H_{\alpha,\beta}}{\sum \Delta H}$$



Thermal Analysis



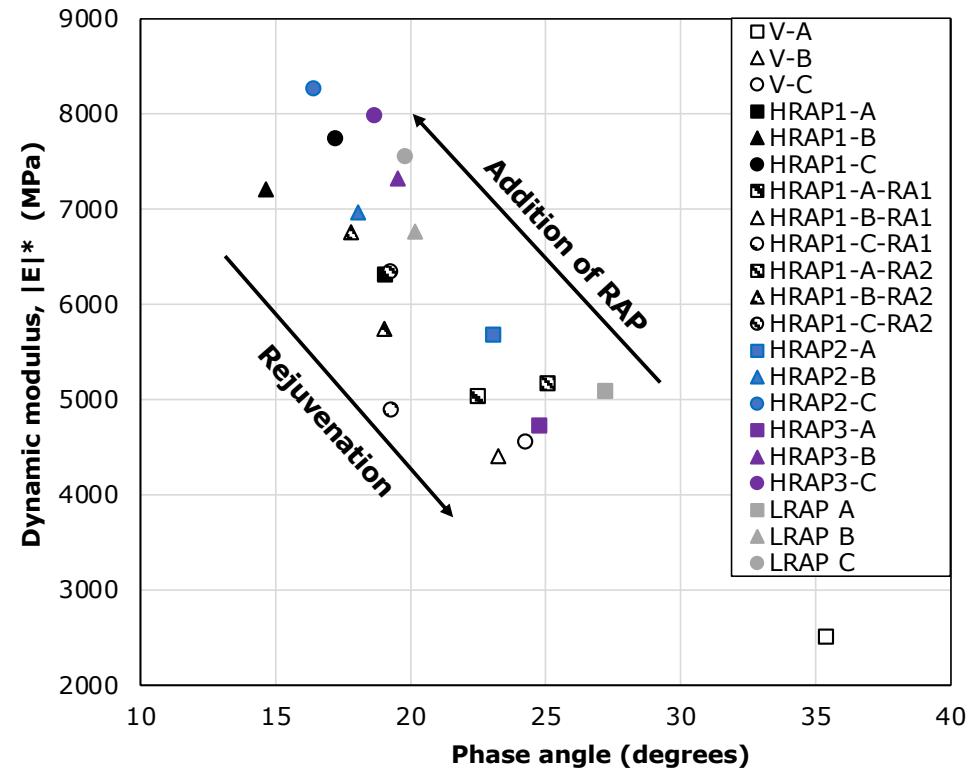
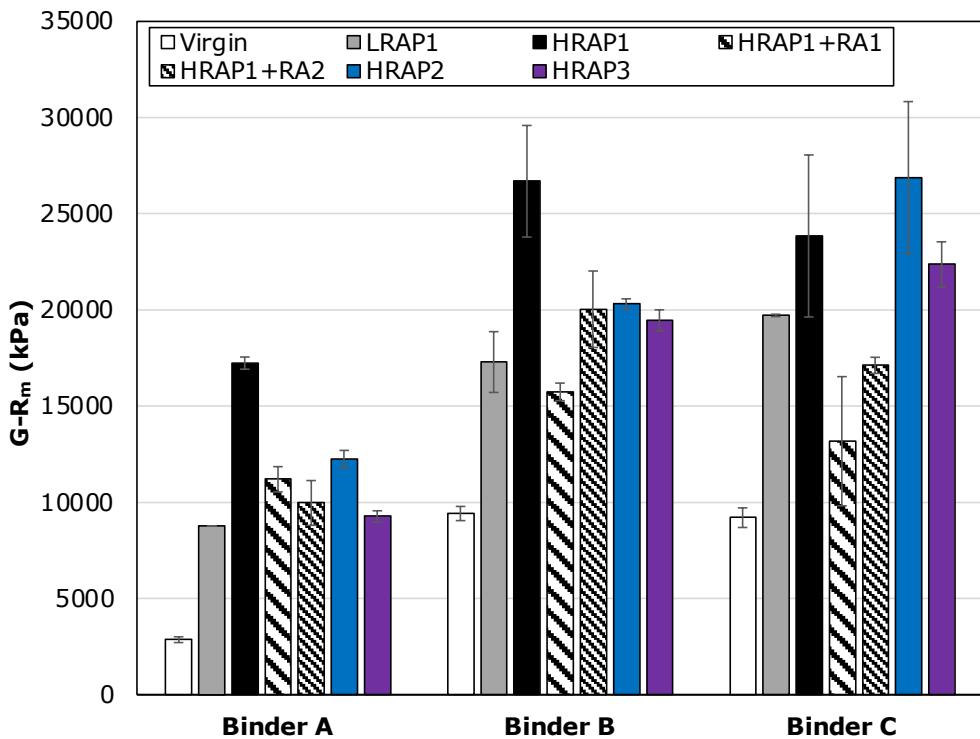
- The increase in RAP content shifted $T_{g\beta}$ to positive temperatures for all three binders
- Inclusion of both RAs reversed this trend, with RA1 generally resulting in a larger reversal indicating its higher effectiveness



Part 2: Mixture Testing Results

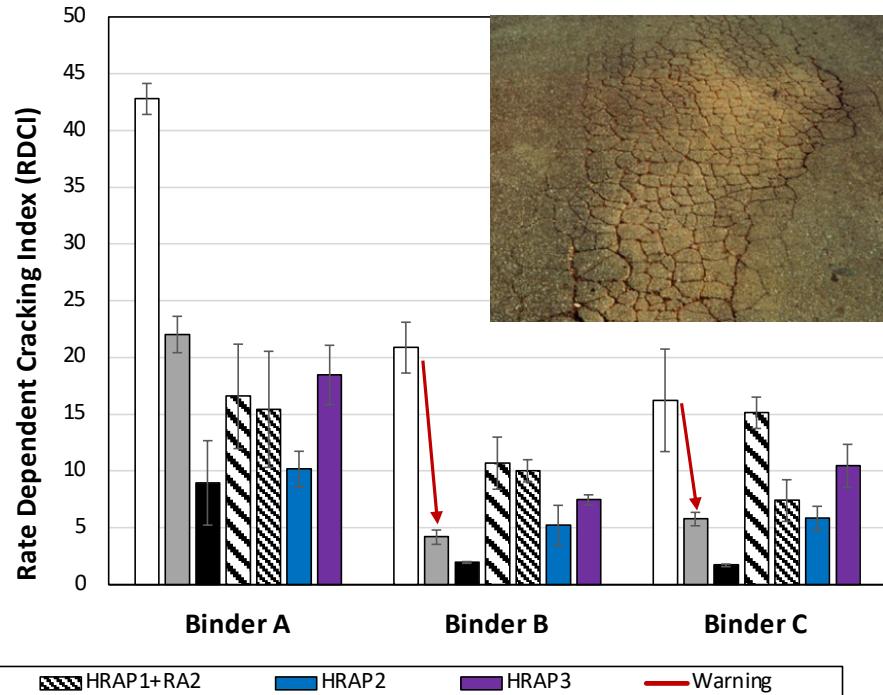
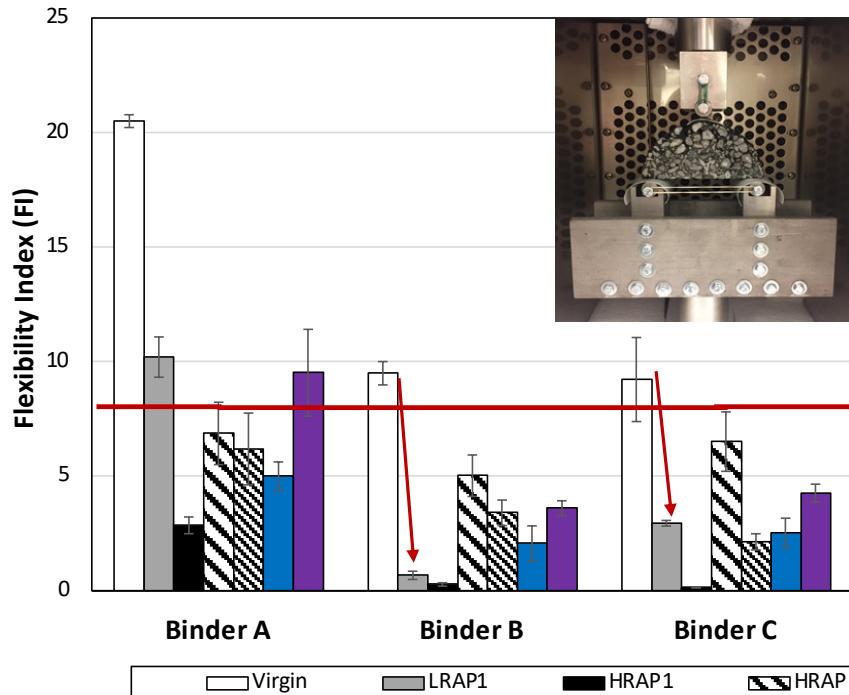


Complex Modulus Testing Results



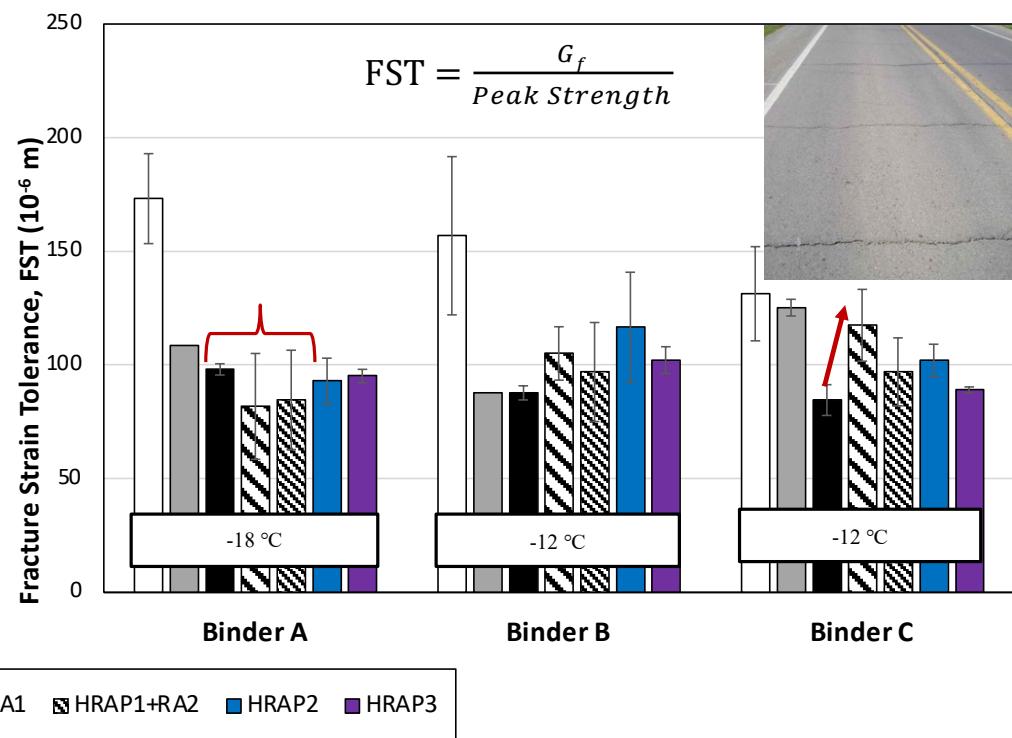
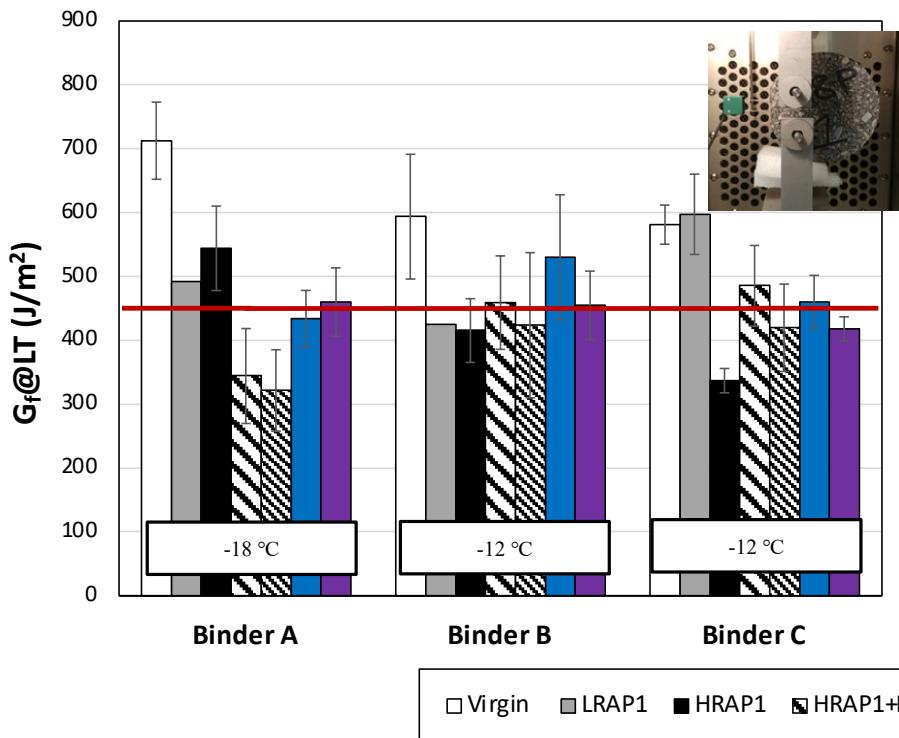
- Mixtures with both RA1 and RA2 show the lower $|E^*|$ and higher δ , however, RA1 generally resulting in a larger reduction indicating its higher effectiveness
- Mixtures with binder B shows lowest compatibility with control RAP and RA

Intermediate Temperature Fracture : I-FIT Test



- Virgin B and C quite similar but the inclusion of RAP shows the difference
- RAP1 still more incompatible with all binders
- RAs improve the fracture performance properties at intermediate temperature, but RA1 showing better or similar performance to RA2

Low-Temperature Fracture: DCT Test



- FST shows that low temperature performance of binder A is not improved by RAs' presence
- RA1 significantly improve low temperature performance of RAP1 mixture with Binder C
- Intermediate temperature performance changes do not translate in exactly same manner to low temperature performance impacts



Part 3 : Statistical Analysis



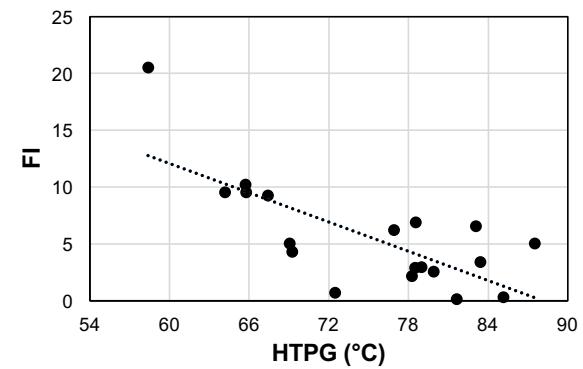
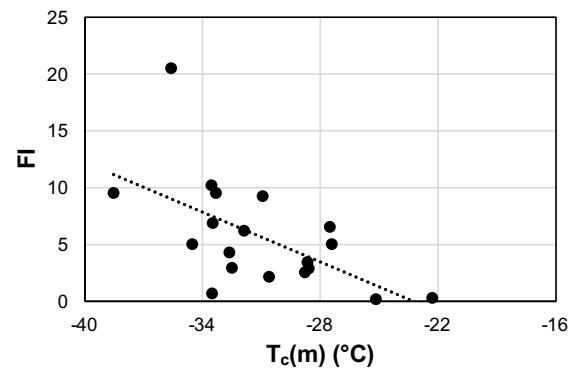
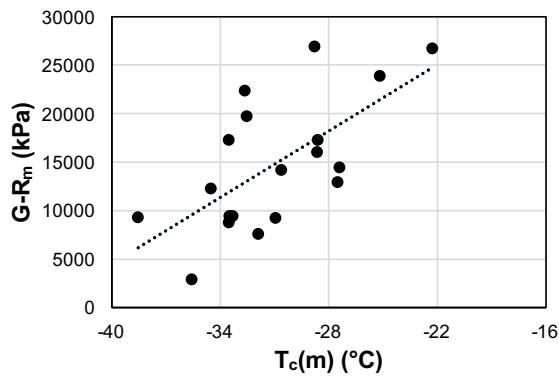
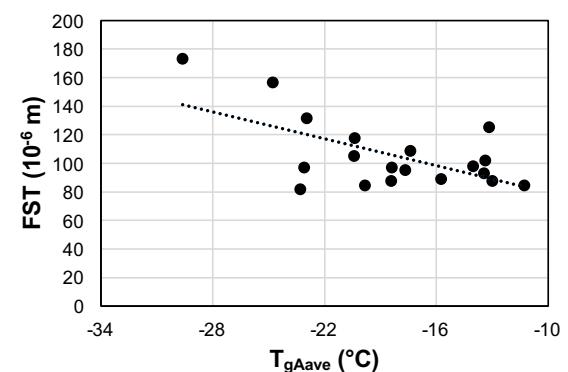
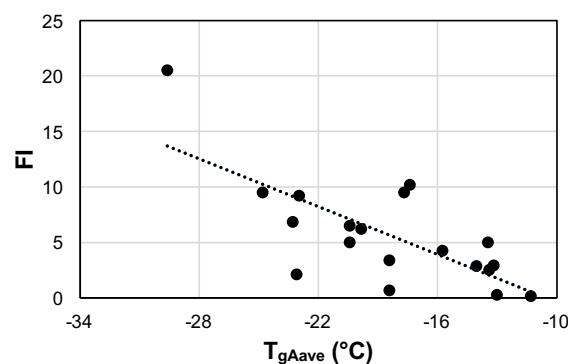
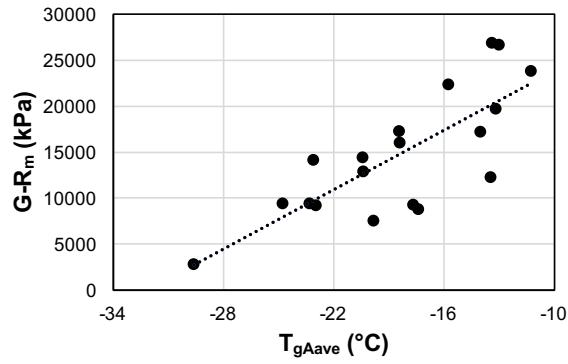
Statistical Analyses: Example

			Mixture Properties				
			Fracture Parameters				Rheological Parameters
			FI	RDCI	G _f @DCT	FST	
Binder Properties	Rheological Parameters	R	0.65	0.62	0.39	0.37	0.51
		T _{c(s)}	0.46	0.48	0.25	0.30	0.52
		T _{c(m)}	0.59	0.58	0.29	0.27	0.66
		ΔT _c	0.45	0.41	0.20	0.13	0.48
		HTPG	0.91	0.90	0.11	0.16	0.84
		LTPG	0.48	0.49	0.27	0.30	0.54
		G-R	0.46	0.45	0.30	0.28	0.54
DSC Parameters	DSC Parameters	T _{gα}	0.36	0.37	0.27	0.42	0.40
		T _{gβ}	0.50	0.52	0.35	0.55	0.52
		T _{gAave}	0.73	0.76	0.41	0.61	0.78
		Φ _α	0.48	0.52	0.21	0.27	0.38
		T _g	0.44	0.44	0.35	0.49	0.48

- FI, RDCI, and G-R_m show the most significant correlation with binder properties
- FST from the DCT test shows good correlation with DSC (glass transition properties)
- T_{gAave} shows a better correlation with most mixture parameters



Correlation Plots: Example



Summary

- **Rheological properties such as G-R, $T_c(m)$, and T_g have indicated that RAP1 is potentially incompatible, whereas RAP2 is potentially compatible, given that both RAPs have comparable PG.**
- **Binder-B showed potential for inferior performance than binder-C (both binders had similar PGs).**
- DSC parameters have consensually captured potential incompatibility of RA2. Therefore, **DSC parameters are recommended** for the compatibility characterization of RAs.
- Results of ΔT_c can be misleading sometimes and thus should be evaluated in conjunction with $T_c(m)$.
- T_{gAave} showed strong correlations with mixture fracture parameters and can potentially be used for preliminary material screening.





Thank you for your attention!

Questions and Comments?

shubham.modi@unh.edu

